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Abstract. The transfer matrix $T(s) = C[I_n s - A]^{-1} B$ of a linear system $\dot{x} = Ax + Bu$, $y = Cx$ can be always written in the standard form $T(s) = \frac{P(s)}{d(s)}$, where $P(s)$ is the polynomial matrix and $d(s)$ is the minimal common denominator. The irreducible transfer matrix is called normal if every nonzero second order minor of $P(s)$ is divisible by $d(s)$. It is shown that for an unnormal transfer matrix of the controllable system there exists a state-feedback gain matrix K such that the closed-loop system transfer matrix $T(s) = C[I_n s - (A + BK)]^{-1} B$ is normal. In the case of the output-feedback the closed-loop transfer matrix $T_c(s) = C[I_n s - (A + BFC)]^{-1} B$ can be made normal only if the system is controllable and observable.

Key words: normalization, transfer matrix, feedback, linear system

1. Introduction and preliminaries

Lampe and Rosenwasser in [5,6] have been investigated relationships between the time-domain description and the frequency-domain description. They have shown, for example, that if the normal transfer matrix is written in the standard form $T(s) = \frac{P(s)}{d(s)}$ ($d(s)$ is the minimal common denominator), then every second order nonzero minor of $P(s)$ is divisible by $d(s)$. In [6] it was shown that cyclic matrices are structurally stable i.e. if the matrix $A \in R^{n \times n}$ is cyclic (the minimal polynomial is equal to the characteristic polynomial) and $A_0 \in R^{n \times n}$ is an arbitrary matrix, there exists a positive number ε_0 such that for all $|\varepsilon| < \varepsilon_0$ the matrix $A + \varepsilon A_0$ is cyclic. Some implications of this approach to electrical circuits have been discussed in [2]. The main subject of this paper is to show that for an unnormal transfer matrix of the controllable system there exists a state-feedback gain matrix K such that the closed-loop system transfer matrix $T_c(s) = C[I_n s - (A + BK)]^{-1} B$ is normal. The normalization of transfer matrix by output-feedbacks will be also considered.

Let $R^{m \times n}$ be the set of $m \times n$ real matrices and $R^n := R^{n \times 1}$.

Consider the linear continuous-time system

$$(1a) \quad \dot{x} = Ax + Bu$$

$$(1b) \quad y = Cx$$

where $x = x(t) \in R^n$ is the state vector, $u = u(t) \in R^m$ and $y = y(t) \in R^p$ are the input and output vectors, respectively and $A \in R^{n \times n}$, $B \in R^{n \times m}$, $C \in R^{p \times n}$. It is assumed that $rank B = m$ and $rank C = p$.

The transfer matrix of the system (1) is given by

$$(2) \quad T(s) = C[I_n s - A]^{-1} B$$

which can be written in the standard form

$$(3) \quad T(s) = \frac{P(s)}{d(s)}$$

where $P \in R^{p \times m}[s], R^{p \times m}[s]$ is the set of $p \times m$ polynomial matrices and $d(s)$ is the minimal common denominator of all entries of $T(s)$.

Using elementary row and column operations we may transform any polynomial matrix $P \in R^{p \times m}[s]$ to its Smith canonical form [3,4]

$$(4) \quad P_s(s) = \text{diag}[i_1(s), i_2(s), \dots, i_r(s), 0, \dots, 0] \in R^{p \times m}[s]$$

where $i_1(s), \dots, i_r(s)$ are monic invariant polynomials satisfying the divisibility condition $i_{k+1}(s) | i_k(s)$, i.e. $i_{k+1}(s)$ is divisible with zero remainder by $i_k(s), k = 1, \dots, r-1$ and $r = \text{rank } P(s)$.

The invariant polynomials can be determined by the relation

$$(5) \quad i_k(s) = \frac{D_k(s)}{D_{k-1}(s)} \quad (D_0(s) = 1), \quad k = 1, \dots, r$$

where $D_k(s)$ is the greatest common divisor of all the $k \times k$ minors of $P(s)$.

The characteristic polynomial $\varphi(s) = \det[I_n s - A]$ of the matrix $A \in R^{n \times n}$ and its minimal polynomial $\Psi(s)$ are related by [1]

$$(6) \quad \Psi(s) = \frac{\varphi(s)}{D_{n-1}(s)}$$

From (4)-(6) it follows that $\Psi(s) = \varphi(s)$ if and only if

$$(7) \quad D_1(s) = D_2(s) = \dots = D_{n-1}(s) = 1$$

A matrix $A \in R^{n \times n}$ satisfying (7) (or equivalently $\Psi(s) = \varphi(s)$) is called cyclic.

2. Normalization of transfer matrix by feedbacks

Consider the system (1) with the state-feedback

$$(8) \quad u = v + Kx, \quad v \in R^m \text{ and } K \in R^{m \times n}$$

Substitution of (11) into (1a) yields

$$(9) \quad \dot{x} = (A + BK)x + Bv$$

The transfer matrix of the closed-loop system is given by

$$(10) \quad T_c(s) = C[I_n s - (A + BK)]^{-1} B$$

The problem of normalization of transfer matrix by state-feedbacks can be stated as follows. Given the system (1) with A not cyclic and the pair (A, C) unobservable. Find a gain matrix K such that the closed-loop transfer matrix (10) is normal.

Theorem 1. Let the matrix A of (1) be not cyclic and the pair (A, C) be unobservable. Then there exists a gain matrix K such that the transfer matrix (10) is normal if and only if the pair (A, B) is controllable.

Proof. Necessity. It is well-known [3,4] that the pair $(A+BK, B)$ is controllable if and only if the pair (A, B) is controllable. If the pair (A, B) is uncontrollable then the transfer matrix (10) is not normal. Thus if the pair (A, B) is uncontrollable then there does not exist K such that the transfer matrix (10) is normal.

Sufficiency. If the pair (A, B) is controllable then there exists a non-singular matrix $T \in R^{n \times n}$ such that

$$(11a) \quad \bar{A} = TAT^{-1} = \begin{bmatrix} A_{11} & \dots & A_{1m} \\ \dots & \dots & \dots \\ A_{m1} & \dots & A_{mm} \end{bmatrix}, \bar{B} = TB = \begin{bmatrix} B_1 \\ \vdots \\ B_m \end{bmatrix}, A_{ij} \in R^{d_i \times d_j}, B_i \in R^{d_i \times m}$$

where

$$(11b) \quad A_{ij} = \begin{cases} \begin{bmatrix} 0 & \dots & I_{d_i-1} \\ \dots & \dots & \dots \\ -a_i & \dots & \dots \end{bmatrix} & \text{for } i = j \\ \begin{bmatrix} 0 \\ \dots \\ -a_{ij} \end{bmatrix} & \text{for } i \neq j \end{cases}, B_i = \begin{bmatrix} 0 \\ \dots \\ b_i \end{bmatrix} \quad a_{ij} = [a_0^{ij} \ a_1^{ij} \ \dots \ a_{d_j-1}^{ij}] \\ b_i = [0 \ \dots \ 0 \ 1 \ b_{i,i+1} \ \dots \ b_{im}]$$

and d_1, \dots, d_m are the controllability indexes satisfying $\sum_{i=1}^{m_1} d_i = n$.

Let

$$(12) \quad \hat{B} = \begin{bmatrix} b_1 \\ b_2 \\ \vdots \\ b_m \end{bmatrix}^{-1} = \begin{bmatrix} 1 & b_{12} & \cdots & b_{1m} \\ 0 & 1 & \cdots & b_{2m} \\ \cdots & \cdots & \cdots & \cdots \\ 0 & 0 & \cdots & 1 \end{bmatrix}^{-1}$$

and

$$(13) \quad K = \begin{bmatrix} K_1 \\ k \end{bmatrix}, K_1 \in R^{(m-1) \times n}, k = [k_1 \ k_2 \ \cdots \ k_n] \in R^{1 \times n}$$

Using (11a) and (12) it is easy to verify that

$$(14) \quad \tilde{B} = \bar{B}\hat{B} = \text{diag}[\tilde{b}_1, \dots, \tilde{b}_m], \tilde{b}_i = [0 \ \cdots \ 0 \ 1]^T \in R^{d_i} \quad (T \text{ denotes the transpose})$$

Define

$$(15) \quad \bar{K} = \hat{B}^{-1}KT^{-1} = \begin{bmatrix} -a_{n_1} + e_{n_1+1} \\ \cdots \\ -a_{n_{m-1}} + e_{n_{m-1}+1} \\ -a_{n_m} - k \end{bmatrix}$$

where $n_i = \sum_{k=1}^i d_k$, a_{n_i} is the n_i -th row of the matrix \bar{A} , e_i is the i -th row of I_n .

Using (15), (17) and (18) it is easy to verify that

$$(16) \quad A_c = T(A+BK)T^{-1} = \bar{A} + \bar{B}\bar{K}T^{-1} = \bar{A} + \tilde{B}\bar{K} = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \cdots & \cdots & \cdots & \cdots & \cdots \\ 0 & 0 & 0 & \cdots & 1 \\ k_1 & k_2 & k_3 & \cdots & k_n \end{bmatrix}$$

The matrix (16) is cyclic and k will be used to make the pair (A_c, C) observable. It can be shown that if A_c has the Frobenius canonical form (16) then it is always possible to choose its entries k_1, \dots, k_n so that the pair (A_c, C) is observable. If the matrix A_c is cyclic, the pair (A_c, B) is controllable and the pair (A_c, C) is observable then the transfer matrix (10) is normal.

If the pair (A, B) is controllable then the gain matrix can be found by the use of the following procedure.

Procedure

Step 1. Compute a non-singular matrix T transforming the pair (A, B) to the canonical form (11) and $\bar{A}, \bar{B}, \hat{B}, \tilde{B}$.

Step 2. Using (15) compute \bar{K} and

$$(17) \quad K = \hat{B}\bar{K}T$$

with unknown row k .

Step 3. Choose the row vector k so that the pair (A_c, C) is observable

Step 4. To find the desired K substitute k (found in Step 3) into (17).

Now let us consider the system (1) with the output-feedback

$$(18) \quad u = v + Fy, \quad F \in R^{m \times p}$$

From (1) and (18) we have

$$(19) \quad \dot{x} = (A + BFC)x + Bv$$

The transfer matrix of the closed-loop system is given by

$$(20) \quad T_c(s) = C[I_n s - (A + BFC)]^{-1} B$$

The problem of normalization of transfer matrix by output-feedbacks can be stated as follows. Given the system (1) with A not cyclic, the pair (A,B) controllable and the pair (A,C) observable. Find a gain matrix F such that the closed-loop transfer matrix (20) is normal.

Note that if the pair (A,C) is unobservable then the pair $(A+BFC,C)$ is also unobservable and the closed-loop transfer matrix (20) is not normal for any gain matrix F . Thus, the normalization problem of transfer matrix by output-feedbacks has a solution only if the pair (A,C) is observable. If additionally the pair (A,B) is controllable the normalization problem is reduced to find a gain matrix such that the closed-loop system matrix $\hat{A}_c = A+BFC$ is cyclic. Let $K = FC$. Then using the approach given in the proof of Theorem 1 we may find K given by (17) such that the matrix $\hat{A}_c = A+BK$ is cyclic. By Kronecker – Capelli theorem the equation $K = FC$ has a solution F for given C and K if and only if

$$(21) \quad \text{rank } C = \text{rank} \begin{bmatrix} C \\ K \end{bmatrix}$$

Therefore, the following theorem has been proved.

Theorem 2. Let the pair (A,B) be controllable, the pair (A,C) be observable and the matrix A of (1) be not cyclic. Then there exists a gain matrix F such that the transfer matrix (20) is normal if and only if the condition (21) is satisfied.

If (21) holds then applying suitable elementary column operations to $K=FC$ we obtain

$$(22) \quad [K_1 \ 0] = F[C_1 \ 0], \quad K_1 \in R^{m \times p}, \quad C_1 \in R^{p \times p}$$

and $\det C_1 \neq 0$ since C by assumption has full row rank. From (22) we have

$$(23) \quad F = K_1 C_1^{-1}$$

3. Concluding remarks

It has been shown that for an unnormal transfer matrix of the controllable system (1) there exists the state-feedback (8) such that the closed-loop transfer matrix (10) is normal. In general case the solution to the problem is not unique. A procedure for computation of the state-feedback gain matrix has been given. Necessary and sufficient conditions have been also established for normalization of the transfer matrix of the system (1) by output-feedbacks. With minor modifications the considerations can be also applied to discrete-time linear systems. An extension of these considerations for singular linear systems will be presented in a next paper. An open problem is an extension of these considerations for standard and singular two-dimensional linear systems [3].

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